## High Accuracy Shock-Fitted Computation of <br> Unsteady Detonation with Detailed Kinetics

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## Outline

- Gas phase detonation introduction
- Length scale requirements from steady traveling wave solutions for $H_{2}$-air (review)
- Unsteady dynamics of ozone detonation


## Fundamentals of Detonation

- Detonation: shockinduced combustion
 process
- applications: aerospace propulsion, safety, military, internal combustion engines, etc.


## Length and Time Scale Discussion

Simplistic linear advection-reaction model:

$$
\begin{gathered}
\underbrace{\frac{\partial \psi}{\partial t}}_{\text {evolution }}+\underbrace{u_{o} \frac{\partial \psi}{\partial x}}_{\text {advection }}=\underbrace{-k \psi}_{\text {reaction }} \\
\frac{d \psi}{d t}=-k \psi: \quad \text { time scale } \quad \tau=\frac{1}{k} \\
u_{o} \frac{d \psi}{d x}=-k \psi: \quad \text { length scale } \quad \ell=\frac{u_{o}}{k}
\end{gathered}
$$

Fast reaction (large $k$ ) induces small length and time scales.

## Motivation

- Detailed kinetics models are widely used in detonation simulations.
- The finest length scale predicted by such models is usually not clarified and often not resolved.
- Tuning computational results to match experiments without first harmonizing with underlying mathematics renders predictions unreliable.
- See Powers and Paolucci, AIAA Journal, 2005.
- We explore the transient behavior of detonations with fully resolved detailed kinetics.


## Verification and Validation

- verification: solving the equations right (math).
- validation: solving the right equations (physics).
- Main focus here on verification
- Some limited validation possible, but detailed validation awaits more robust measurement techniques.
- Verification and validation always necessary but never sufficient: finite uncertainty must be tolerated.


## Model: Steady 1D Reactive Euler Equations

$$
\begin{gathered}
\rho u=\rho_{o} D \\
\rho u^{2}+p=\rho_{o} D^{2}+p_{o} \\
e+\frac{u^{2}}{2}+\frac{p}{\rho}=e_{o}+\frac{D^{2}}{2}+\frac{p_{o}}{\rho_{o}} \\
p=\rho \Re T \sum_{i=1}^{N} \frac{Y_{i}}{M_{i}}, \\
e=\sum_{i=1}^{N} Y_{i}\left(h_{i, f}^{o}+\int_{T_{o}}^{T} c_{p i}(\hat{T}) d \hat{T}-\frac{\Re T}{M_{i}}\right) \\
\frac{d Y_{i}}{d x}=\frac{M_{i}}{\rho_{o} D} \sum_{j=1}^{J} \nu_{i j} A_{j} T^{\beta_{j}} e^{\left(\frac{-E_{j}}{\Re T}\right)}(\underbrace{\prod_{k=1}^{N}\left(\frac{\rho Y_{k}}{M_{k}}\right)^{\nu_{k j}^{\prime}}}_{\text {forward }}-\underbrace{\frac{1}{K_{j}^{c}} \prod_{k=1}^{N}\left(\frac{\rho Y_{k}}{M_{k}}\right)^{\nu_{k j}^{\prime \prime}}}_{\text {reverse }})
\end{gathered}
$$

## Eigenvalue Analysis of Local Length Scales

Algebraic reduction yields

$$
\frac{d \mathbf{Y}}{d x}=\mathbf{f}(\mathbf{Y})
$$

Local behavior is modeled by

$$
\frac{d \mathbf{Y}}{d x}=\mathbf{J} \cdot\left(\mathbf{Y}-\mathbf{Y}^{*}\right)+\mathbf{b}, \quad \mathbf{Y}\left(x^{*}\right)=\mathbf{Y}^{*}
$$

whose solution is

$$
\mathbf{Y}(x)=\mathbf{Y}^{*}+\left(\mathbf{P} \cdot e^{\boldsymbol{\Lambda}\left(x-x^{*}\right)} \cdot \mathbf{P}^{-1}-\mathbf{I}\right) \cdot \mathbf{J}^{-1} \cdot \mathbf{b}
$$

Here, $\boldsymbol{\Lambda}$ has eigenvalues $\lambda_{i}$ of Jacobian $\mathbf{J}$ in its diagonal. Length scales given by

$$
\ell_{i}(x)=\frac{1}{\left|\lambda_{i}(x)\right|} .
$$

## Computational Methods: Steady Detonation

- A standard ODE solver (DLSODE) was used to integrate the equations.
- Standard IMSL subroutines were used to evaluate the local Jacobians and eigenvalues at every step.
- The Chemkin software package was used to evaluate kinetic rates and thermodynamic properties.
- Computation time was typically one minute on a 1 GHz HP Linux machine.


## Physical System

- Hydrogen-air detonation: $2 \mathrm{H}_{2}+\mathrm{O}_{2}+3.76 \mathrm{~N}_{2}$.
- $N=9$ molecular species, $L=3$ atomic elements, $J=19$ reversible reactions.
- $p_{o}=1 \mathrm{~atm}$.
- $T_{o}=298 \mathrm{~K}$.
- Identical to system studied by both Shepherd (1986) and Mikolaitis (1987).


## Detailed Kinetics Model

| $j$ | Reaction | $A_{j}$ | $\beta_{j}$ | $E_{j}$ |
| ---: | :--- | :--- | ---: | ---: |
| 1 | $H_{2}+O_{2} \rightleftharpoons O H+O H$ | $1.70 \times 10^{13}$ | 0.00 | 47780 |
| 2 | $O H+H_{2} \rightleftharpoons H_{2} O+H$ | $1.17 \times 10^{9}$ | 1.30 | 3626 |
| 3 | $H+O_{2} \rightleftharpoons O H+O$ | $5.13 \times 10^{16}$ | -0.82 | 16507 |
| 4 | $O+H_{2} \rightleftharpoons O H+H$ | $1.80 \times 10^{10}$ | 1.00 | 8826 |
| 5 | $H+O_{2}+M \rightleftharpoons H O_{2}+M$ | $2.10 \times 10^{18}$ | -1.00 | 0 |
| 6 | $H+O_{2}+O_{2} \rightleftharpoons H O_{2}+O_{2}$ | $6.70 \times 10^{19}$ | -1.42 | 0 |
| 7 | $H+O_{2}+N_{2} \rightleftharpoons H O_{2}+N_{2}$ | $6.70 \times 10^{19}$ | -1.42 | 0 |
| 8 | $O H+H O_{2} \rightleftharpoons H_{2} O+O_{2}$ | $5.00 \times 10^{13}$ | 0.00 | 1000 |
| 9 | $H+H O_{2} \rightleftharpoons O H+O H$ | $2.50 \times 10^{14}$ | 0.00 | 1900 |
| 10 | $O+H O_{2} \rightleftharpoons O_{2}+O H$ | $4.80 \times 10^{13}$ | 0.00 | 1000 |
| 11 | $O H+O H \rightleftharpoons O+H_{2} O$ | $6.00 \times 10^{8}$ | 1.30 | 0 |
| 12 | $H_{2}+M \rightleftharpoons H+H+M$ | $2.23 \times 10^{12}$ | 0.50 | 92600 |
| 13 | $O_{2}+M \rightleftharpoons O+O+M$ | $1.85 \times 10^{11}$ | 0.50 | 95560 |
| 14 | $H+O H+M \rightleftharpoons H_{2} O+M$ | $7.50 \times 10^{23}$ | -2.60 | 0 |
| 15 | $H+H O_{2} \rightleftharpoons H_{2}+O_{2}$ | $2.50 \times 10^{13}$ | 0.00 | 700 |
| 16 | $H O_{2}+H O_{2} \rightleftharpoons H_{2} O_{2}+O_{2}$ | $2.00 \times 10^{12}$ | 0.00 | 0 |
| 17 | $H_{2} O_{2}+M \rightleftharpoons O H+O H+M$ | $1.30 \times 10^{17}$ | 0.00 | 45500 |
| 18 | $H_{2} O_{2}+H \rightleftharpoons H O_{2}+H_{2}$ | $1.60 \times 10^{12}$ | 0.00 | 3800 |
| 19 | $H_{2} O_{2}+O H \rightleftharpoons H_{2} O+H O_{2}$ | $1.00 \times 10^{13}$ | 0.00 | 1800 |

## Temperature Profile



- Temperature flat in the post-shock induction zone $0<x<$ $2.6 \times 10^{-2} \mathrm{~cm}$.
- Thermal explosion followed by relaxation to equilibrium at
$x \sim 10^{0} \mathrm{~cm}$.


## Mole Fractions versus Distance

- significant evolution at fine length scales $x<$ $10^{-3} \mathrm{~cm}$.
- results agree with those of Shepherd.

Eigenvalue Analysis: Length Scale Evolution

- Finest length scale:
$2.3 \times 10^{-5} \mathrm{~cm}$.

- Coarsest length scale
$3.0 \times 10^{1} \mathrm{~cm}$.
- Finest length scale similar to that necessary for numerical stability of ODE solver.


## Verification: Comparison with Mikolaitis



- Lagrangian calculation allows direct comparison with Mikolaitis' results.
- agreement very good.


## Grid Convergence

- Finest length scale must be resolved to converge at proper order.
- Results are converging at proper order for first and second order discretizations.


## Numerical Stability



- Discretizations finer than finest physical length scale are numerically stable.
- Discretizations coarser than finest physical length scale are numerically unstable.


## Unsteady Model: Reactive Euler Equations

- one-dimensional,
- inviscid,
- detailed mass action kinetics with Arrhenius temperature dependency,
- ideal mixture of calorically imperfect ideal gases


## Model: Unsteady Reactive Euler PDEs

$$
\begin{aligned}
\frac{\partial \rho}{\partial t}+\frac{\partial}{\partial x}(\rho u) & =0, \\
\frac{\partial}{\partial t}(\rho u)+\frac{\partial}{\partial x}\left(\rho u^{2}+p\right) & =0, \\
\frac{\partial}{\partial t}\left(\rho\left(e+\frac{u^{2}}{2}\right)\right)+\frac{\partial}{\partial x}\left(\rho u\left(e+\frac{u^{2}}{2}+\frac{p}{\rho}\right)\right) & =0, \\
\frac{\partial}{\partial t}\left(\rho Y_{i}\right)+\frac{\partial}{\partial x}\left(\rho u Y_{i}\right) & =M_{i} \dot{\omega}_{i}, \\
p & =\rho \Re T \sum_{i=1}^{N} \frac{Y_{i}}{M_{i}}, \\
e & =e\left(T, Y_{i}\right), \\
\dot{\omega}_{i} & =\dot{\omega}_{i}\left(T, Y_{i}\right) .
\end{aligned}
$$

## Computational Method

- Shock fitting coupled with a fifth order method for continuous regions
- Fifth order WENO5M for spatial discretization
- Fifth order Runge-Kutta for temporal discretization
- see Henrick, Aslam, Powers, J. Comp. Phys., 2006, for full details on shock fitting


## Outline of Shock Fitting Method

- Transform from lab frame to shock-attached frame, $(x, t) \rightarrow(\xi, \tau)$
- example mass equation becomes

$$
\frac{\partial \rho}{\partial \tau}+\frac{\partial}{\partial \xi}(\rho(u-D))=0
$$

- In interior
- fifth order WENO5M for spatial discretization
- fifth order Runge-Kutta for temporal discretization


## Outline of Shock Fitting Method, cont.

- At shock boundary, one-sided high order differences are utilized
- Note that some form of an approximate Riemann solver must be used to determine the shock speed, $D$, and thus set a valid shock state
- At downstream boundary, a zero gradient (constant extrapolation) approximation is utilized


## Summary of Shock-Fitting Method



## Difficulties in Unsteady Calculations

- Note that $H_{2}$-air steady detonation had length scales spanning six orders of magnitude
- This is feasible for steady calculations but extremely challenging in a transient calculation.
- To cleanly illustrate the challenges of coupled length and time scales, we choose a realistic problem with less stiffness that we can verify and validate: ozone detonation.


## Ozone Reaction Kinetics

| Reaction | $A_{j}^{f}, A_{j}^{r}$ | $\beta_{j}^{f}, \beta_{j}^{r}$ | $E_{j}^{f}, E_{j}^{r}$ |
| :---: | :---: | :---: | :---: |
| $O_{3}+M \leftrightarrows O_{2}+O+M$ | $6.76 \times 10^{6}$ | 2.50 | $1.01 \times 10^{12}$ |
|  | $1.18 \times 10^{2}$ | 3.50 | 0.00 |
| $O+O_{3} \leftrightarrows 2 O_{2}$ | $4.58 \times 10^{6}$ | 2.50 | $2.51 \times 10^{11}$ |
|  | $1.18 \times 10^{6}$ | 2.50 | $4.15 \times 10^{12}$ |
| $O_{2}+M \leftrightarrows 2 O+M$ | $5.71 \times 10^{6}$ | 2.50 | $4.91 \times 10^{12}$ |
|  | $2.47 \times 10^{2}$ | 3.50 | 0.00 |

see Margolis, J. Comp. Phys., 1978, or Hirschfelder, et al., J. Chem. Phys., 1953.

## Validation: Comparison with Observation

- Streng, et al., J. Chem. Phys., 1958.
- $p_{o}=1.01325 \times 10^{6}$ dyne $/ \mathrm{cm}^{2}, T_{o}=298.15 \mathrm{~K}$, $Y_{O_{3}}=1, Y_{O_{2}}=0, Y_{O}=0$.

| Value | Streng, et al. | this study |
| :---: | :---: | :---: |
| $D_{C J}$ | $1.863 \times 10^{5} \mathrm{~cm} / \mathrm{s}$ | $1.936555 \times 10^{5} \mathrm{~cm} / \mathrm{s}$ |
| $T_{C J}$ | 3340 K | 3571.4 K |
| $p_{C J}$ | $3.1188 \times 10^{7}$ dyne $/ \mathrm{cm}^{2}$ | $3.4111 \times 10^{7}$ dyne $/ \mathrm{cm}^{2}$ |

Slight overdrive to preclude interior sonic points.

## Stable Strongly Overdriven Case: Length Scales

$$
D_{o}=2.5 \times 10^{5} \mathrm{~cm} / \mathrm{s}
$$



## Mean-Free-Path Estimate

- The mixture mean-free-path scale is the cutoff minimum length scale associated with continuum theories.
- A simple estimate for this scale is given by Vincenti and Kruger, '65:

$$
\ell_{m f p}=\frac{M}{\sqrt{2} \mathcal{N} \pi d^{2} \rho} \sim 10^{-7} \mathrm{~cm} .
$$

## Stable Strongly Overdriven Case: Mass Fractions

$$
D_{o}=2.5 \times 10^{5} \mathrm{~cm} / \mathrm{s}
$$



## Stable Strongly Overdriven Case: Temperature

$$
D_{o}=2.5 \times 10^{5} \mathrm{~cm} / \mathrm{s}
$$



## Stable Strongly Overdriven Case: Pressure

$$
D_{o}=2.5 \times 10^{5} \mathrm{~cm} / \mathrm{s}
$$



## Stable Strongly Overdriven Case: Transient

 Behavior for Various Resolutions Initialize with steady structure of $D_{o}=2.5 \times 10^{5} \mathrm{~cm} / \mathrm{s}$.

## 3 Cases Near Neutral Stability: Transient Behavior



## Slightly Unstable Case: Transient Behavior

Initialized with steady structure, $D_{o}=2.4 \times 10^{5} \mathrm{~cm} / \mathrm{s}$.


## Case After Bifurcation: Transient Behavior

Initialized with steady structure of $D_{o}=2.1 \times 10^{5} \mathrm{~cm} / \mathrm{s}$.


## Long Time $D_{\max } / D_{0}$ versus $D_{C J} / D_{0}$



## Effect of Resolution on Unstable Moderately

## Overdriven Case

| $\Delta x$ | Numerical Result |
| :---: | :---: |
| $1 \times 10^{-7} \mathrm{~cm}$ | Unstable Pulsation |
| $2 \times 10^{-7} \mathrm{~cm}$ | Unstable Pulsation |
| $4 \times 10^{-7} \mathrm{~cm}$ | Unstable Pulsation |
| $8 \times 10^{-7} \mathrm{~cm}$ | $O_{2}$ mass fraction $>1$ |
| $1.6 \times 10^{-6} \mathrm{~cm}$ | $O_{2}$ mass fraction $>1$ |

- Algorithm failure for insufficient resolution
- At low resolution, one misses critical dynamics


## Examination of $H_{2}$-Air Results

| Reference | $\ell_{\text {ind }}(\mathrm{cm})$ | $\ell_{f}(\mathrm{~cm})$ | $\Delta x(\mathrm{~cm})$ | Under-resolution |
| :---: | :---: | :--- | :--- | :--- |
| Oran, et al., 1998 | $2 \times 10^{-1}$ | $2 \times 10^{-4}$ | $4 \times 10^{-3}$ | $2 \times 10^{1}$ |
| Jameson, et al., 1998 | $2 \times 10^{-2}$ | $5 \times 10^{-5}$ | $3 \times 10^{-3}$ | $6 \times 10^{1}$ |
| Hayashi, et al., 2002 | $2 \times 10^{-2}$ | $1 \times 10^{-5}$ | $5 \times 10^{-4}$ | $5 \times 10^{1}$ |
| Hu, et al., 2004 | $2 \times 10^{-1}$ | $2 \times 10^{-4}$ | $3 \times 10^{-3}$ | $2 \times 10^{1}$ |
| Powers, et al., 2001 | $2 \times 10^{-2}$ | $3 \times 10^{-5}$ | $8 \times 10^{-5}$ | $3 \times 10^{0}$ |
| Osher, et al., 1997 | $2 \times 10^{-2}$ | $3 \times 10^{-5}$ | $3 \times 10^{-2}$ | $1 \times 10^{3}$ |
| Merkle, et al., 2002 | $5 \times 10^{-3}$ | $8 \times 10^{-6}$ | $1 \times 10^{-2}$ | $1 \times 10^{3}$ |
| Sislian, et al., 1998 | $1 \times 10^{-1}$ | $2 \times 10^{-4}$ | $1 \times 10^{0}$ | $5 \times 10^{3}$ |
| Jeung, et al., 1998 | $2 \times 10^{-2}$ | $6 \times 10^{-7}$ | $6 \times 10^{-2}$ | $1 \times 10^{5}$ |

All are under-resolved, some severely.

## Conclusions

- Unsteady detonation dynamics can be accurately simulated when sub-micron scale structures admitted by detailed kinetics are captured with ultra-fine grids.
- Shock fitting coupled with high order spatial discretization assures numerical corruption is minimal.
- Predicted detonation dynamics consistent with results from one-step kinetic models.
- At these length scales, diffusion will play a role and should be included in future work.


## Moral

You either do detailed kinetics with the proper resolution,

or

you are fooling yourself and others, in which case you should stick with reduced kinetics!

