

# EE566 Solid State Devices

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Dept of Electrical Engineering

University of Notre Dame

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## Assignment 5 SOLUTIONS

Problem 1: 5.11

|   |   |
|---|---|
| p | n |
|---|---|

$1.2 \Omega\text{-cm}$     $0.2 \Omega\text{-cm}$   
 $\tau_n = 10^{-6} \text{ s}$     $\tau_p = 10^{-8} \text{ s}$

From Fig. 1.15.

$\rho_p = 1.2 \Omega\text{-cm}$ ,    $P = 1.5 \times 10^{16} \text{ cm}^{-3}$   
 $\rho_n = 0.2 \Omega\text{-cm}$ ,    $n = 2.9 \times 10^{16} \text{ cm}^{-3}$

ASSNS

$$V_{bi} = \frac{kT}{q} \ln \frac{N_d N_A}{n_i^2}$$

suppose fully ionized,  $N_d = n$ ,  $N_A = P$

$$\therefore V_{bi} = \frac{kT}{q} \ln \frac{nP}{n_i^2} = \frac{1.8 \times 10^{-23} \times 300}{1.6 \times 10^{-19}} \ln \frac{1.5 \times 10^{16} \times 2.9 \times 10^{16}}{(1.45 \times 10^{10})^2}$$
$$= 0.722 \text{ (V)}$$

(b)  $n_{p0} = \frac{n_i^2}{P} = \frac{(1.45 \times 10^{10})^2}{1.5 \times 10^{16}} = 1.39 \times 10^4 \text{ cm}^{-3}$

$$P_{n0} = \frac{n_i^2}{n} = \frac{(1.45 \times 10^{10})^2}{2.9 \times 10^{16}} = 7.25 \times 10^3 \text{ cm}^{-3}$$

with applied bias:

$$n_p = n_{p0} \left( \exp \frac{qV}{kT} - 1 \right) = 1.35 \times 10^4 \text{ cm}^{-3}$$
$$P_n = P_{n0} \left( \exp \frac{2V}{kT} - 1 \right) = 7.06 \times 10^{13} \text{ cm}^{-3}$$

(c)  $J_0 = q n_i^2 \left( \frac{D_p}{N_d L_p} + \frac{D_n}{N_A L_n} \right) = q n_i^2 \left( \frac{1}{N_d} \sqrt{\frac{D_p}{\tau_p}} + \frac{1}{N_A} \sqrt{\frac{D_n}{\tau_n}} \right)$

$$= 1.6 \times 10^{-19} \times (1.45 \times 10^{10})^2 \left( \frac{1}{1.5 \times 10^{16}} \sqrt{\frac{12.3}{10^{-8}}} + \frac{1}{1.5 \times 10^{16}} \sqrt{\frac{34.6}{10^{-6}}} \right)$$
$$= 5.587 \times 10^{-11} \text{ A/cm}^2$$

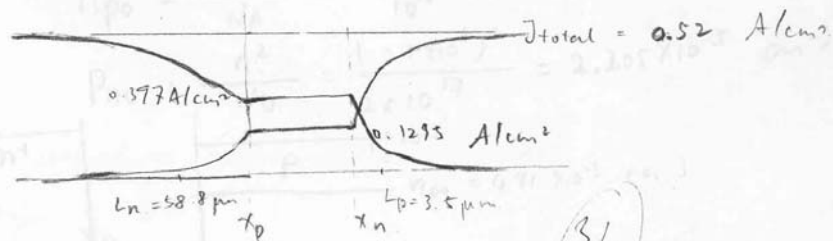
on p-side

$$J = J_n \text{ (at } x_p) = q D_n \frac{n_i^2}{N_A L_n} (e^{qV_0/kT} - 1)$$
$$= 1.6 \times 10^{-19} \times 34.6 \times \frac{(1.45 \times 10^{10})^2}{1.5 \times 10^{16} \times \sqrt{34.6 \times 10^{-6}}} (e^{23} - 1)$$
$$= 0.1285 \text{ A/cm}^2$$

on n-side

$$J_p \text{ (at } x_n) = q D_p \frac{n_i^2}{N_D L_p} (e^{qV_0/kT} - 1)$$
$$= 1.6 \times 10^{-19} \times 12.3 \times \frac{(1.45 \times 10^{10})^2}{2.9 \times 10^{16} \times \sqrt{12.3 \times 10^{-8}}} (e^{23} - 1)$$
$$= 0.397 \text{ A/cm}^2$$

$$J_{\text{total}} = J_0 (e^{qV_0/kT} - 1) = 5.387 \times 10^{-11} (e^{23} - 1)$$
$$= 0.52 \text{ A/cm}^2$$



(d) on n-side,

$$J_p = J_p \text{ (at } x_n) \cdot \exp\left(-\frac{x - x_n}{L_p}\right)$$

$$\text{when } J_p = J_n, \rightarrow J_p = \frac{1}{2} J_{\text{total}}$$

$$0.397 \times \exp\left(-\frac{x - x_n}{L_p}\right) = \frac{1}{2} \times 0.52$$

$$x - x_n = 1.48 \mu\text{m}$$

$$W = \sqrt{2 \frac{\epsilon_s}{\epsilon_0} (V_{bi} - V_a) \left( \frac{1}{N_A} + \frac{1}{N_D} \right)}$$

$$= \sqrt{2 \times 11.7 \times 8.85 \times 10^{-14} \times 10^{16} \times 0.7382 - 0.589 \times 10^{16} \times \left( \frac{1}{1.5} + \frac{1}{3.0} \right)}$$

$$\approx 0.13 \mu\text{m} \quad N_A \cdot x_p = N_D \cdot x_n$$

$$\Rightarrow x_n = 0.045 \mu\text{m}, x_p = 0.09 \mu\text{m}$$

when  $J_{maj} = J_{tot} - J_{min} \Rightarrow J_{min} = \frac{1}{2} J_{tot} = 0.247 \text{ A/cm}^2$

$$\therefore J_p(x) = 0.3790 \cdot e^{-\frac{x-x_n}{L_p}}$$

$$= 0.247$$

$\Rightarrow x = 1.4 \mu\text{m}$  from the  $x_n$  into the n-type region.

problem 2

a)  $J_0 = q \left( \frac{D_n n_{p0}}{L_n} + \frac{D_p p_{n0}}{L_p} \right) = q n_i^2 \left( \frac{D_n}{L_n N_A} + \frac{D_p}{L_p N_D} \right)$   $D_n = 200 \text{ cm}^2/\text{s}$   $D_p = 10 \text{ cm}^2/\text{s}$

$$L_n = \sqrt{D_n \tau_n} = 0.0063 \text{ cm}$$

$$n_i \approx 2.1 \times 10^6 \text{ cm}^{-3}$$

$$L_p = \sqrt{D_p \tau_p} = 0.0014 \text{ cm}$$

$$\therefore J_0 = 2.2365 \times 10^{-7} \text{ A/cm}^2$$

b) in the p-side  $P = N_A$   $n_p = n_{p0} \cdot e^{\frac{qV_a}{kT}}$   $e^{-\frac{x}{L_n}} = \frac{n_i^2}{N_A} \cdot e^{\frac{qV_a}{kT}} \cdot e^{-\frac{x}{L_n}}$

in the n-side  $n = N_D$   $p_n = p_{n0} \cdot e^{-\frac{qV_a}{kT}}$   $e^{-\frac{x}{L_p}} = \frac{n_i^2}{N_D} \cdot e^{-\frac{qV_a}{kT}} \cdot e^{-\frac{x}{L_p}}$

$$V_a = 0V$$

$$P = N_A$$

$$n_p = n_{p0}$$

$$p_n = p_{n0}$$

$$-x_p \quad x=0 \quad x_n$$

$$V_a = 0.5V$$

$$P = N_A$$

$$n_{p0}$$

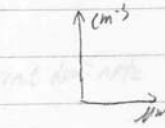
$$n_p$$

$$L_n$$

$$L_p$$

$$n = N_D$$

$$p_{n0}$$



c). Outside depletion region in n-type

$$J_p = q n_i^2 \frac{D_p}{N_A L_p} (e^{\frac{qV_b}{kT}} - 1) e^{-\frac{x-x_n}{L_p}} \approx 7.7 \times 10^{-12} e^{-\frac{x-x_n}{L_p}} \quad x > x_n$$

Outside depletion region in p-type

$$J_n = q n_i^2 \frac{D_n}{N_A L_n} (e^{\frac{qV_b}{kT}} - 1) e^{\frac{x+x_p}{L_n}} = 6.9 \times 10^{-9} e^{\frac{x+x_p}{L_n}} \quad x < -x_p$$

$$W = \sqrt{\frac{2 \epsilon_s}{q} (V_{bi} - V_a) \left( \frac{1}{N_A} + \frac{1}{N_D} \right)}$$

$$V_{bi} = \frac{kT}{q} \ln \frac{N_A N_D}{n_i^2}$$

$$\Rightarrow W = 0.81 \mu\text{m}$$

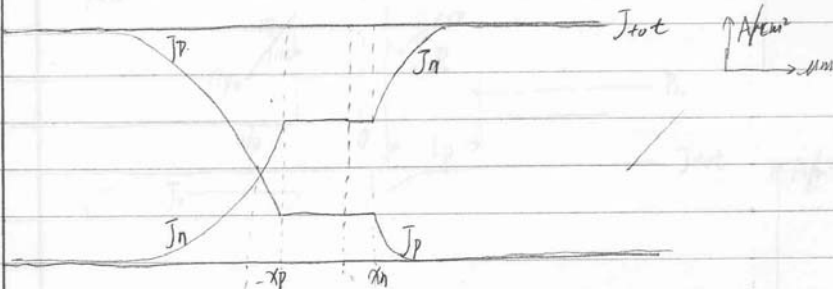
At the junction  $x=0$ ,  $E(0) = \frac{2(V_{bi} - V_a)}{W} = 16.75 \text{ kV/cm}$

$$J_{\text{recombination}} = \frac{q n_i}{2\tau} \cdot \frac{kT}{q E(0)} \exp\left(\frac{qV_a}{2kT}\right) = 7.16 \times 10^{-8} \text{ A/cm}^2$$

Inside the depletion region, the minority current is constant

$$i. J_{\text{tot}} = J_r + J_n(x=-x_p) + J_p(x=x_n)$$

$$= 7.16 \times 10^{-8} + 7.7 \times 10^{-12} + 6.9 \times 10^{-9} = 7.86 \times 10^{-8} \text{ A/cm}^2$$



← majority current dominate.

in n-type majority current dominate →

minority current dominate

d). In the p-type region.  $L_n = \sqrt{D_n \tau_n} = \sqrt{200 \times 0.2 \times 10^{-6}} = 0.0063 \text{ cm} \approx 63 \mu\text{m} \gg W_B$

$$\therefore \Delta n(x) = \frac{n_i^2}{N_A} \left( \frac{x+x_p}{W_B-x_p} + 1 \right) \left( e^{\frac{qV_A}{kT}} - 1 \right) \quad n(x) = \Delta n(x) + n_{p0}$$

$$\therefore N_A x_p = W_B x_n$$

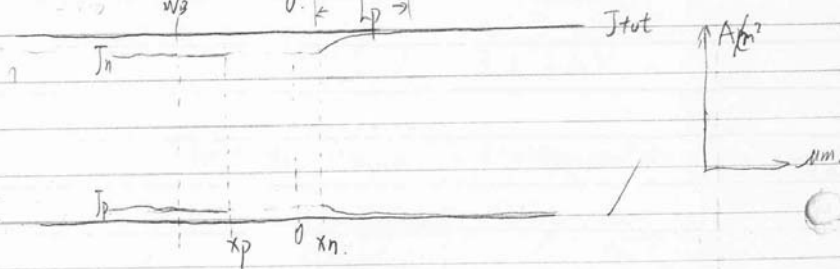
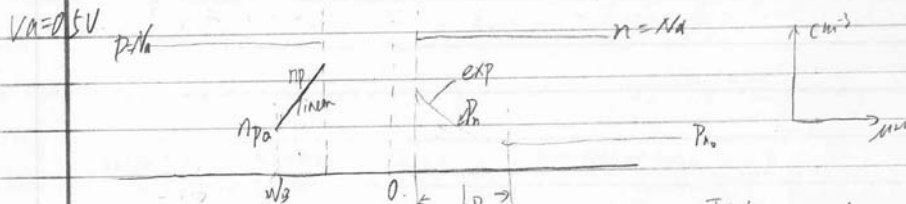
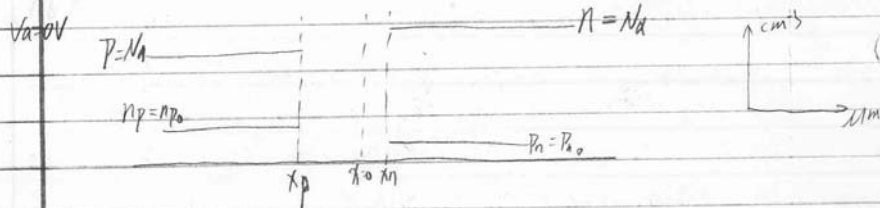
$$\therefore x_p \approx W = 0.8 \mu\text{m} ; \int_{x_p}^{x_n} N_A dx \gg J_p(x=x_n)$$

$$J_n = q D_n \frac{dn(x)}{dx} = \frac{q n_i^2 D_n}{N_A (W_B - x_p)} \left( e^{\frac{qV_A}{kT}} - 1 \right) \quad \text{where } x_p \approx W = 0.8 \mu\text{m}$$

$$\Rightarrow J_n(x=x_p) \approx 3.3 \times 10^7 \text{ A/cm}^2$$

$$J_{rec} \text{ is not changed. } J_{rec} = 7.16 \times 10^{-8} \text{ A/cm}^2$$

$$J = J_n + J_p + J_{rec} \approx 4.0 \times 10^7 \text{ A/cm}^2$$



e. The current in long base diode is much smaller than the current in short base diode.

The reason is in long base diode  $WB \approx L$ , therefore most minority carrier has been combined before they reach the contact. While in short diode,  $WB \ll L$ . Therefore most minority carrier can get through the base without recombination. When they reach the contact, the current increase.

6/16

Handwritten scribble

Since it is n-p junction, electrons diffuse from n to p region

$$J_n = \frac{qD_n}{L_n} n_{i0} \exp\left(\frac{qV}{kT}\right) \left(\frac{L_n}{W}\right)$$

to increase  $J_n$ , in fact keep the doping same and introducing  $qV$

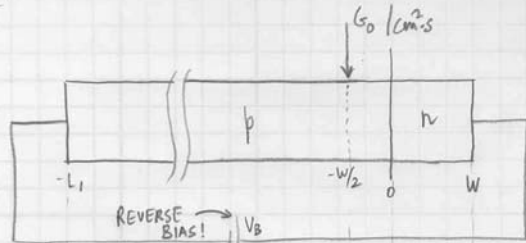
$$\exp\left(\frac{qV}{kT}\right) = 0.119 \text{ eV}$$

$$qV = kT \ln(0.119) = 11.63 \times 10^{-3} \times 0.119 = 0.138 \text{ eV}$$

$$V = 0.119 \text{ V}$$

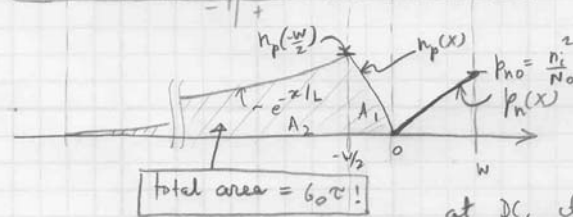
ASSGN 5, Prob 3  
 PROBLEM 5.10(MKC)

(a) There are a few tricks that no one used to solve this problem 😊



FIRST, note that the generation rate is in  $\text{cm}^{-2}\text{s}$ , & NOT  $\text{cm}^{-3}\text{s}$  !!

So  $n_p(-w/2) \neq G_0\tau$ , UNITS ARE WRONG!



To find  $n_p(-w/2)$ , we note that at DC, the total excess electrons in the p-region is given by the area

$$\frac{1}{2} n_p(-w/2) \times w/2 + n_p(-w/2) \int_0^{L_1} dx e^{-x/L} = G_0\tau$$

$$\Rightarrow n_p(-w/2) = \frac{G_0\tau}{L \times (1 - e^{-L/L}) + w/4} \approx \frac{G_0\tau}{L + w/4}$$

$\approx 0$  since  $L_1 \gg L$ .

$$n_p(-w/2) \approx \frac{G_0\tau}{L + w/4} \quad \text{NOW the units are right!}$$

(b)  $\therefore$  Current with illumination is ( $@ x = 0$ ),

$$J_{tot}^{ill} = J_n^{diff} + J_p^{diff} = qG_0 \left[ \frac{2D\tau}{w(w+L)} \right] + \frac{qDn_i^2}{N_0W}$$

$$|J_{tot}^{ill}| = \frac{qD}{W} \left[ \frac{2G_0\tau}{(w/4+L)} + \frac{n_i^2}{N_0} \right]$$

(c) Steady S. Current without illumination is just revers-bias leakage

$$|J_{tot}^{noill}| = qD \left[ \frac{n_i^2}{N_0L} + \frac{n_i^2}{N_0W} \right] = \frac{qDn_i^2}{N_0} \left[ \frac{1}{L} + \frac{1}{W} \right] \approx \frac{qDn_i^2}{N_0W}$$

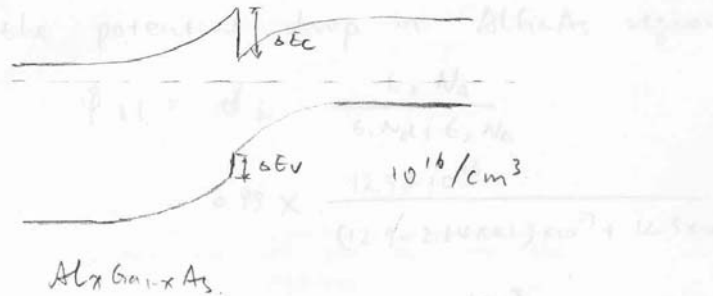
$$|J_{tot}^{noill}| \approx \frac{qDn_i^2}{N_0W}$$

Problem 4

For  $\text{Al}_x\text{Ga}_{1-x}\text{As} / \text{GaAs}$  heterojunction:

when  $x < 0.45$ , electron affinity:  $\chi = 4.07 - 1.1x$  eV

$\text{GaAs}$ ,  $\chi = 4.07$  eV



Since it is n<sup>+</sup>p junction, electrons injected from n<sup>+</sup> to p region

$$J_n = - \frac{q D_n}{L_n} \frac{n_{i1}^2}{N_{A1}} \exp\left(\frac{\Delta E_g}{kT}\right) \left[ \exp\left(\frac{qV_a}{kT}\right) - 1 \right]$$

to increase by 100, we can keep the doping same and introducing  $\Delta E_g$

$$\exp\left(\frac{\Delta E_g}{kT}\right) = 0.119 \text{ eV}$$

$$E_{g\text{AlGaAs}} - E_{g\text{GaAs}} = 1.155x + 0.37x^2 = 0.48 \text{ eV}$$

$$x = 0.1$$

$$\phi_i = \chi_2 - \chi_1 + \frac{E_{g2}}{q} - \frac{kT}{q} \ln \frac{N_{c1} N_{v2}}{N_{d1} N_{a2}}$$

$$= -1.1 \times 0.1 + 1.42 - \frac{kT}{q} \ln \frac{1.9 \times 10^{17} \times 9.5 \times 10^{18}}{10^{17} \times 10^{16}}$$

$$= -0.11 + 1.42 - 0.312$$

$$= 0.99 \text{ eV}$$

the potential drop in AlGaAs region:

$$\phi_{i1} = \phi_i \cdot \frac{\epsilon_2 N_a}{\epsilon_1 N_d + \epsilon_2 N_a}$$

$$= 0.99 \times \frac{12.9 \times 10^{16}}{(12.9 - 2.64 \times 0.1) \times 10^{17} + 12.9 \times 10^{16}}$$

$$\phi_{i1} = 0.99 \times \frac{12.9}{12.6 \times 10 + 12.9}$$

$$= 0.09 \text{ eV}$$

$$\phi_{i2} = 0.9 \text{ eV}$$

In AlGaAs,

$$\frac{q N_d \lambda_n^2}{2 \epsilon_1} = 0.09 \text{ eV}, \quad \lambda_n = \sqrt{\frac{0.09 \times 2 \times 12.6 \times \epsilon_0}{1.6 \times 10^{-19} \times 10^{23}}}$$

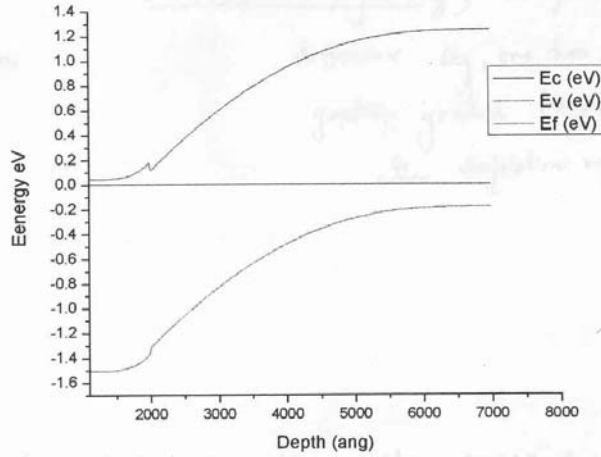
$$\lambda_n = 3.54 \times 10^{-8} \text{ m} = 35.4 \text{ nm}$$

In GaAs

$$\frac{q N_d \lambda_p^2}{2 \epsilon_2} = 0.9 \text{ eV}, \quad \lambda_p = \sqrt{\frac{0.9 \times 2 \times 12.9 \times \epsilon_0}{1.6 \times 10^{-19} \times 10^{22}}}$$

$$\lambda_p = 3.58 \times 10^{-7} \text{ m} = 358 \text{ nm}$$

With  $i-v$  posn., for  $Al_{0.1}Ga_{0.9}As / GaAs$  with doping of  $1 \times 10^{17}/cm^3$  and  $1 \times 10^{16} cm^{-3}$ , we can see the  $\Delta E_c$  is not very big.

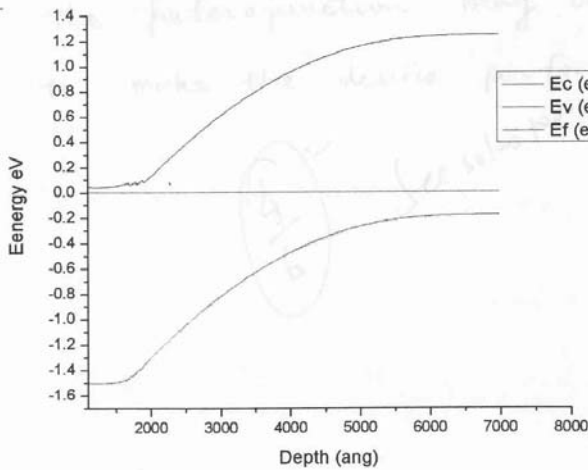


If I add 3 gradient layer to the structure, the  $\Delta E_c$  kink could be removed:

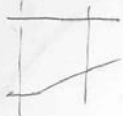
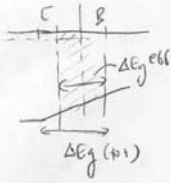
$GaAs$   
 $Al_{0.16}Ga_{0.84}As$  30nm  
 $Al_{0.04}Ga_{0.96}As$  30nm  
 $Al_{0.07}Ga_{0.93}As$  30nm  
 $Al_{0.1}Ga_{0.9}As$

$N_A = 1 \times 10^{16} / cm^3$   
 $N_D = 1 \times 10^{17} / cm^3$

try 'graded' structure - too...



(c)



Since the  $\frac{\Delta E_g}{kT}$  factor depends upon the  $\Delta E_g$  across the E-B depletion region only, to get all the bandgap difference  $\Delta E_g$ , one has to ensure that the ~~graded~~ graded layer lies entirely inside the depletion region.

(d) for heterojunction, the current is high

The disadvantage is: require epitaxial growth, thus increasing cost.

The heterojunction may contain defects to make the device performance worse.



~~See solution 10~~

$$J_0 = q n_i^2 \left( \frac{D_n}{N_A L_p} + \frac{D_p}{N_D L_n} \right) = q n_i^2 \left( \frac{1}{N_A} \sqrt{\frac{D_n}{\tau_p}} + \frac{1}{N_D} \sqrt{\frac{D_p}{\tau_n}} \right)$$

$$= 1.6 \times 10^{-17} (4.5 \times 10^{16})^2 \left( \frac{1}{10^{16}} \sqrt{\frac{25}{10^{-8}}} + \frac{1}{10^{16}} \sqrt{\frac{10}{10^{-8}}} \right)$$

$$= 3.587 \times 10^{-11} \text{ A/cm}^2$$