

UNIVERSITY OF NOTRE DAME
DEPARTMENT OF AEROSPACE AND MECHANICAL ENGINEERING

Professor H.M. Atassi
113 Hessert Center
Tel: 631-5736
Email: atassi.1@nd.edu

AME-562
Mathematical Methods II

One Dimensional Piston Problem

1 Governing equations

Consider a one-dimensional duct aligned with the x -axis. To the right of the piston, the duct is full with a gas at rest. At time $t=0$ the piston starts moving with a velocity $u_p(t)$. Let ρ , u , and s describe the gas density, velocity and entropy. We assume an isentropic process and therefore the gas properties are governed by the two first order partial differential equations:

$$\frac{\partial \rho}{\partial t} + u \frac{\partial \rho}{\partial x} + \rho \frac{\partial u}{\partial x} = 0 \quad (1)$$

$$\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + \frac{c^2}{\rho} \frac{\partial \rho}{\partial x} = 0 \quad (2)$$

where c is the speed of sound. We assume the piston position is given by the function $X(t)$. The initial conditions are

$$t \leq 0, \quad u = 0, \quad c = c_0 \quad (3)$$

and the boundary conditions are,

$$t > 0, \quad u(X(t), t) = u_p = \dot{X}(t). \quad (4)$$

2 Characteristics Equations

$$I_+ : \frac{dx}{dt} = u + c \quad C_+ \quad (5)$$

$$I_- : \frac{dx}{dt} = u - c \quad C_- \quad (6)$$

$$II_+ : du + \frac{c}{\rho} d\rho = 0 \quad \text{on } C_+ \quad (7)$$

$$II_- : du - \frac{c}{\rho} d\rho = 0 \quad \text{on } C_- \quad (8)$$

Note that since the gas is isentropic, $(\gamma - 1)\frac{d\rho}{\rho} = 2\frac{dc}{c}$. Therefore (7-8) can be rewritten as

$$II_+ : du + \frac{2}{\gamma - 1}dc = 0 \text{ on } C_+ \quad (9)$$

$$II_- : du - \frac{2}{\gamma - 1}dc = 0 \text{ on } C_- \quad (10)$$

Integrating 9 along C_+ and 10 along C_- , gives

$$II_+ : u + \frac{2}{\gamma - 1}c = r^*, \text{ on } C_+ \quad (11)$$

$$II_- : u - \frac{2}{\gamma - 1}c = s^*, \text{ on } C_- \quad (12)$$

where r^* and s^* constant along C_+ and C_- , respectively. r^* and s^* are known as the Riemann invariants.

3 Simple Waves

If one of the Riemann invariants is constant throughout the domain, the solution corresponds to a wave motion in *only* one direction. In the present problem,

$$u = \frac{r^* + s^*}{2} \quad (13)$$

$$c = \frac{\gamma - 1}{2}(r^* - s^*) \quad (14)$$

In general, the value of u and c will depend on the two parameters (r^*, c^*) indicating two waves where the information is propagating along the two families of characteristics. On the other hand, if $s^* = \text{constant}$ everywhere, then u and c receive information from the characteristic C_+ only through the variation of r^* from one characteristic to another. Problems reduced to simple waves are much simpler to solve.

3.1 Proposition

The solution in a region adjacent to a constant state is always a simple wave solution.

4 Solution

We construct the solution assuming no breaking will occur. This will be examined later.

4.1 Steady State Region: $t > 0, x > c_0 t$

Along C_+ originating from the positive x-axis,

$$u + \frac{2}{\gamma - 1}c = \frac{2}{\gamma - 1}c_0 \quad (15)$$

Similarly along C_- originating from the positive x-axis,

$$u - \frac{2}{\gamma - 1}c = -\frac{2}{\gamma - 1}c_0 \quad (16)$$

These equations imply that for the region $x > c_0 t$, we have

$$u = 0 \quad c = c_0 \quad (17)$$

The characteristics in this region are straight lines whose equations are

$$x - x_0^+ = c_0 t \quad \text{along } C_+ \quad (18)$$

$$x - x_0^- = -c_0 t \quad \text{along } C_-, \quad (19)$$

where x_0^+ and x_0^- are the points of their intersection with the x-axis. Note in this region there no waves and the gas remain quiescent.

4.2 Simple Wave Solution

All characteristics C_- will originate from the positive x-axis. Thus they have the same Riemann invariant as (16) shows. This means that we have the following relationship

$$u = \frac{2}{\gamma - 1}(c - c_0). \quad (20)$$

Equation 20 is valid everywhere in the field, assuming no shocks. Substituting 20 into 15 show that both u and c are constant along C_+ originating from the piston surface. Hence, we have

$$u = u_p = \dot{X}(t) \quad (21)$$

$$c = c_p \quad (22)$$

Since both u and c are constant along C_+ we can integrate 5,

$$x = X(\tau) + (u_p + c_p)(t - \tau) \quad (23)$$

or

$$x = X(\tau) + \left(c_0 + \frac{\gamma + 1}{2}\dot{X}(\tau)\right)(t - \tau) \quad (24)$$

5 Piston Moving with a Constant Speed (-V)

Substituting \dot{X} by $-V$, we get

$$x = -Vt + (c_0 - \frac{\gamma+1}{2}V)(t - \tau) \quad (25)$$

$$u = -V \quad (26)$$

$$c = c_0 - \frac{\gamma-1}{2}V \quad (27)$$

In the fan region defined by

$$(c_0 - \frac{\gamma+1}{2}V)t < x < tc_0,$$

we have

$$\frac{dx}{dt} = u + c = c_0 + \frac{\gamma+1}{2}u \quad (28)$$

Moreover along C_+ , $c + \frac{\gamma-1}{2}u = \text{constant}$. Therefore u and c are constant. As a result,

$$x = (c_0 + \frac{\gamma+1}{2}u)t \quad (29)$$

and

$$u = \frac{2}{\gamma+1}(\frac{x}{t} - c_0) \quad (30)$$

$$c = \frac{2}{\gamma+1}c_0 + \frac{\gamma-1}{\gamma+1}\frac{x}{t} \quad (31)$$

6 Breaking

It is easy to show that breaking will occur if $\ddot{X} < 0$.