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## Compressibility Effects on Airfoil Lift

The Prandtl-Glauert rule gives

$$C_p = \frac{C_{p,0}}{\sqrt{1 - M_\infty^2}} \tag{1}$$

$$C_{\ell} = \frac{C_{\ell,0}}{\sqrt{1 - M_{\infty}^2}} \tag{2}$$

$$C_m = \frac{C_{m,0}}{\sqrt{1 - M_\infty^2}} \tag{3}$$

The Karman-Tsien rule gives

$$C_p = \frac{C_{p,0}}{\sqrt{1 - M_{\infty}^2} + [M_{\infty}^2 / (1 + \sqrt{1 - M_{\infty}^2})]C_{p,0}/2},\tag{4}$$

and the Laitone's rule states

$$C_p = \frac{C_{p,0}}{\sqrt{1 - M_{\infty}^2} + \left(M_{\infty}^2 \{1 + [(\gamma - 1)/2]M_{\infty}^2)\}/2\sqrt{1 - M_{\infty}^2}\right)C_{p,0}},\tag{5}$$



Figure 1: Comparison of measured lift-curve slope for NACA 4412 profile with Prandtl-Glauert rule.



Figure 2: Comparison of measured lift-curve slope for a propeller section of 6% thickness with Prandtl-Glauert rule.



Figure 3: Compressibility corrections for  $C_p$  compared with experimental results for a NACA 4412 airfoil at an angle of attack of  $\alpha = 1^o 53'$ .  $C_p$  is measured at 0.30-chord location.



Figure 4: Flow past a circular arc profile.

- (a) Streamlines.
- (b) Effect of  $M_{\infty}$  on lift coefficient.
- (c)Low critical Mach number as a function of camber.



Figure 5: The Critical Mach number. Point A is the location of minimum pressure (maximum velocity) on the top surface of the airfoil



Figure 6: Determination of the critical Mach number.

- (B)  $C_p$ . (C)  $C_{p,cr}$ . (D)Intersection gives critical Mach number.



Figure 7: Effect of airfoil thickness on critical Mach number.



Figure 8: Sketch of the variation of profile drag coefficient with free-stream Mach number, illustrating the critical and drag-divergence Mach numbers and showing the large drag rise near Mach 1.



Figure 9: NACA 64-series airfoil compared with a supercritical airfoil at cruise conditions.



Figure 10: The drag-divergence properties of a standard NACA 64-series airfoil and a supercritical airfoil.